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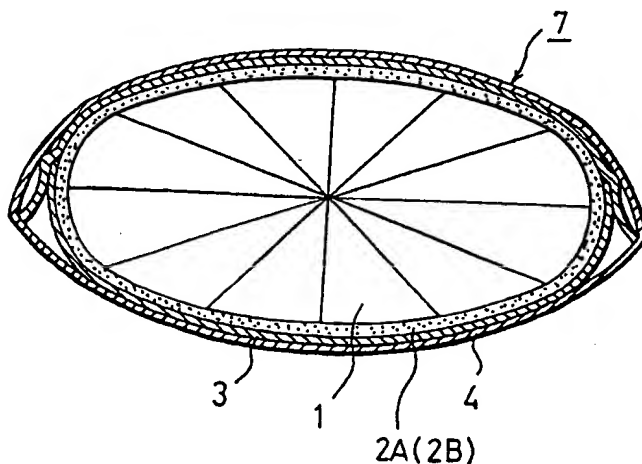
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(54) Heat-resistant expansive member.

(57) The present invention relates to a heat-resistant expansive member suitably used as a holding member for holding a ceramic monolithic catalyst in a motor vehicle or the like. The heat-resistant expansive member of the present invention is made at the blending ratio of 1 to 5 wt% of sepiolite, 30 to 60 wt% of treated vermiculite, 20 to 40 wt% of ceramic fibers and 5 to 20 wt% of an organic binder, or at the blending ratio of 21 to 30 wt% of sepiolite, 30 to 40 wt% of treated vermiculite, 20 to 40 wt% of ceramic fibers and 5 to 20 wt% of an organic binder. Regardless of the low- or high-temperature zone, the heat-resistant expansive member of the present invention presents a great holding force to the monolithic catalyst or the like. The heat-resistant expansive member is improved in cushioning properties and gas-attack resisting properties particularly in the high-temperature zone.

Fig.1



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## Heat-Resistant Expansive Member

Background of the Invention

## 1. Field of the Invention

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The present invention relates to a heat-resistant expansive member in the form of, for example, a sheet preferable as a holding member of a ceramic honeycomb monolithic catalyst forming a catalyst converter in a low pollution engine capable of purifying the emission by oxidizing or reducing harmful components discharged from an automotive engine such as carbon monoxide, hydrocarbon and nitrogen oxides.

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## 2. Description of the Prior Art

The ceramic honeycomb monolithic catalyst excellent in high temperature characteristic is considered to be preferred as the catalyst for achieving a low pollution engine by purifying the emission by oxidizing or reducing the harmful components discharged from an automotive engine such as carbon monoxide, hydrocarbon and nitrogen oxides.

Since the ceramics are brittle and inferior in toughness, the ceramic catalyst is installed, as surrounded by a cushioning holding member, in a metallic casing in order to prevent the ceramic catalyst from being damaged due to a mechanical shock such as vibration occurring during the vehicle is running.

The ceramic honeycomb monolithic catalyst is exposed to the high temperature emission of the engine, and therefore the holding member is required to have an excellent heat resistance so as not to be lowered in the high temperature strength. Further, since the emission is gradually heightened in temperature as the engine runs continuously, the holding member is thermally expanded depending on the temperature increase. Even in such circumstances, it is required that the holding force and cushioning properties for the ceramic honeycomb monolithic catalyst are not lowered.

As the holding member of the monolithic catalyst capable of satisfying such requirements, there is known, for example, the heat-resistant expansive sheet disclosed in the Japanese Patent Publication 61-35143.

This heat-resistant expansive sheet is composed of 40 to 65 wt% of treated vermiculite as obtained by treating particulate vermiculite with an aqueous solution of ammonium dihydrogen phosphate, 25 to 50 wt% of inorganic fibers, and 5 to 15 wt% of a binder selected from the group consisting of inorganic binders.

Table 2 and Fig. 3, to be given later, show the results of tests conducted on this heat-resistant expansive sheet by the present inventor. As apparent from Table 2 and Fig. 3, the heat-resistant expansive sheet above-mentioned presents a relatively great negative expansion due to a creep phenomenon around 200°C to 300°C (more specifically, 200°C to 325°C) corresponding to the low temperature zone. Further, the thermal expansion amount at a temperature of 350°C to 400°C corresponding to the intermediate temperature zone, is considerably small. This causes the monolithic catalyst to be loosened, so that the holding force to the ceramic honeycomb monolithic catalyst is extremely lowered.

Also apparent from Table 2 and Fig. 3, this heat-resistant expansive sheet is restrained in thermal expansion at a temperature of 600°C or more corresponding to the high-temperature zone, thereby to lower the holding force to the ceramic honeycomb monolithic catalyst. Thus, in the conventional heat-resistant expansive sheet, a high holding force may not be expected in both low- and high-temperature zones, causing the monolithic catalyst to be readily loosened.

Further, since this conventional heat-resistant expansive sheet is retained in shape with an inorganic binder only, that part of the holding member exposed to the exhaust gas flowing at a high temperature at a high speed, may gradually fall down. Accordingly, the monolithic catalyst holding performance disappears with the passage of time. That is, this conventional sheet presents the problem that the gas-attack resisting properties are very poor.

There is also known a heat-resistant expansive sheet as obtained by treating the particulate vermiculite mentioned earlier with sodium dihydrogen phosphate. In this sheet, the negative expansion in the low-temperature zone may be restrained, but the thermal expansion at the intermediate- and high-temperature zones is small. Thus, a sufficient holding force may not be expected (See Table 2 and Fig. 3).

It is noted that Applicant has filed an application for such a heat-resistant expansive member under U.S. Appl. 313,548.

Summary of the Invention

In view of the foregoing, the present invention is proposed with the object of providing a heat-resistant expansive member which assures a great holding force from a low-temperature zone to a high-temperature zone, thereby to prevent the monolithic catalyst from being loosened due to a mechanical shock such as vibration or the like occurring while the motor vehicle travels, and which also assures cushioning properties particularly in the high-temperature zone, thereby to prevent the ceramic honeycomb monolithic catalyst from being damaged, and which is improved in gas-attack resisting properties, thereby to prevent the decrease in holding performance with the passage of time.

It is another object of the present invention to provide a heat-resistant expansive member which starts expanding even in the low-temperature zone, assuring a great holding force to the monolithic catalyst from the low-temperature zone to the high-temperature zone.

To achieve the objects above-mentioned, the heat-resistant expansive member in accordance with an embodiment of the present invention contains 1 to 5 wt% of sepiolite, 30 to 60 wt% of treated vermiculite, 20 to 40 wt% of ceramic fibers, and 5 to 20 wt% of an organic binder.

The heat-resistant expansive member having the arrangement above-mentioned contains 1 to 5 wt% of sepiolite, thereby to decrease a negative expansion caused by a creep phenomenon occurring in the low-temperature zone around 300°C. This improves the holding force in the low-temperature zone. Further, the heat-resistant expansive member of the present invention is increased not only in heat resistance in the high-temperature zone of 600°C or more, but also in shape retention to improve the gas-attack resisting properties. Further, the heat-resistant expansive member of the present invention contains 30 to 60 wt% of treated vermiculite. This improves not only the cushioning properties capable of effectively relaxing a mechanical shock such as vibration or the like, but also the expansion amount and expansion force for assuring the holding force. This holding force is gradually increased toward the high-temperature zone of 600°C or more since the heat-resistant expansive member starts expanding at a temperature as low as 275°C. Accordingly, regardless of the low- or high-temperature zone, the heat-resistant expansive member of the present invention may properly hold, with a great holding force, the ceramic honeycomb monolithic catalyst fragile and poor in toughness such that the monolithic catalyst is not loosened. It is therefore possible to prevent the ceramic honeycomb monolithic catalyst from being damaged when a mechanical shock such as vibration or the like is applied thereto during the motor vehicle travels. More specifically, the treated vermiculite is contained in an amount considerably greater than that of sepiolite, so that the heat-resistant expansive member is particularly increased in expansion amount and expansion force and assures moderate gas-attack resisting properties. Accordingly, the heat-resistant expansive member is suitable for a holding member of the catalyst converter for a four-wheel motor vehicle exposed to the exhaust gas of which flowing speed is being slightly lowered, although the compressive strength of the ceramic honeycomb monolithic catalyst is great and the metallic casing is thick so that the catalyst converter has great rigidity. Further, the heat-resistant expansive member contains 20 to 40 wt% of ceramic fibers. This increases the heat resistance of the heat-resistant expansive member, thereby to prevent the occurrence of negative expansion in the low-temperature zone. Further, the ceramic fibers serve as a binder to improve the holding properties of the heat-resistant expansive member particularly in the high temperature zone where the organic binder perfectly disappears. Further, the heat-resistant expansive member contains 5 to 20 wt% of an organic binder, thus improving the shape retention at an ordinary temperature to assure handling convenience.

To achieve the objects above-mentioned, the heat-resistant expansive member in accordance with another embodiment of the present invention contains 21 to 30 wt% of sepiolite, 30 to 40 wt% of treated vermiculite, 20 to 40 wt% of ceramic fibers, and 5 to 20 wt% of an organic binder.

This heat-resistant expansive member contains 21 to 30 wt% of sepiolite, thereby to decrease the negative expansion thereof due to a creep phenomenon occurring in the low-temperature zone around 300°C. This improves the holding force of the heat-resistant expansive member in the low-temperature zone. Also, this heat-resistant expansive member is increased in heat resistance in the high-temperature zone of 600°C or more, thereby to assure a great holding force. Moreover, the shape retention of the heat-resistant expansive member is considerably increased, assuring excellent gas-attack resisting properties. Further, this heat-resistant expansive member contains 30 to 40 wt% of treated vermiculite. This improves not only the cushioning properties for effectively relaxing a mechanical shock such as vibration or the like, but also the expansion amount and expansion force for assuring a holding force. Such a holding force is gradually increased in the high-temperature zone of 600°C or more because of the expansion of the heat-resistant expansive member which has started from 275°C. Accordingly, regardless of the low- or high-temperature zone, this heat-resistant expansive member may properly hold, with a great holding force, the

ceramic honeycomb monolithic catalyst fragile and poor in toughness such that the monolithic catalyst is not loosened. It is therefore possible to prevent the ceramic honeycomb monolithic catalyst from being damaged when a mechanical shock such as vibration or the like is applied thereto during the motor vehicle travels. More specifically, the blending amount of the sepiolite is considerably increased to restrain the expansion amount and expansion force, while improving the heat resistance and shape retention, assuring excellent gas-attack resisting properties. Accordingly, this heat-resistant expansive member is suitable for a holding member of the catalyst converter for a two-wheel motor vehicle exposed to the exhaust gas flowing at a high speed, although the compressive strength of the ceramic honeycomb monolithic catalyst is small and the metallic casing is thin so that the catalyst converter has small rigidity. Likewise in the heat-resistant expansive member previously mentioned, 20 to 40 wt% of ceramic fibers contained in this heat-resistant expansive member prevent the occurrence of negative expansion in the low-temperature zone. Further, the ceramic fibers serve as a binder to improve the holding properties of the heat-resistant expansive member particularly in the high temperature zone. Further, 5 to 20 wt% of the organic binder contained in this heat-resistant expansive member improves the shape retention at an ordinary temperature to assure handling convenience.

According to the present invention, the heat-resistant expansive member preferably contains treated vermiculite as obtained by treating particulate vermiculite with an aqueous solution of sodium ammonium hydrogen phosphate. The particulate vermiculite contains cations apt to be exchanged with  $\text{Na}^+$  ions, and cations apt to be exchanged with  $\text{NH}_4^+$  ions. Accordingly, when the particulate vermiculite is immersed in the aqueous solution above-mentioned containing these both ions, the cations in the particulate vermiculite are effectively ion-exchanged in the aqueous solution. By such an ion exchange, the expansion amount and expansion force of the vermiculite are further increased even in the low-temperature zone.

Other features and effects of the present invention will be readily understood from the following description of embodiments thereof.

#### Brief Description of the Drawings

- Figure 1 is a schematic section view of an example of a catalyst converter;  
 Figure 2 is a schematic front view of a thermal expansion measuring apparatus;  
 Figure 3 is a graph showing the coefficients of thermal expansion of vermiculite treated with different solutions;  
 Figure 4 is a section view of apparatus for measuring the holding force of a heat-resistant expansive sheet;  
 Figure 5 is a graph comparatively showing measurement results of holding force;  
 Figure 6 is a schematic side view of apparatus for testing gas-attack resisting properties; and  
 Figure 7 is a schematic plan view of the apparatus in Figure 6.

#### Detailed Description of the Preferred Embodiments

Fig. 1 is a schematic section view of an example of a catalyst converter. In Fig. 1, a ceramic honeycomb monolithic catalyst 1 is surrounded by a heat-resistant expansive sheet 2A or 2B and mounted on a two-half metallic casing 3. A metallic band 4 fastens the outer periphery of the casing 3.

The heat-resistant expansive sheet 2A according to a first invention may be manufactured by the beater seating method at the blending ratio of 1 to 5 wt% of sepiolite, 30 to 60 wt% of treated vermiculite, 20 to 40 wt% of ceramic fibers, and 5 to 20 wt% of an organic binder. The two-half metallic casing 3 and the metallic band 4 are made of SUS 304.

The sepiolite forming the heat-resistant expansive sheet 2A is available in two types depending on the degree of crystallization. That is, the fibrous type with high degree of crystallization is called  $\alpha$ -sepiolite, while the powder type with low degree of crystallization or amorphous state is called  $\beta$ -sepiolite. Since the  $\beta$ -sepiolite is in the form of powder and is inferior in interlocking performance with ceramic fibers or vermiculite, the  $\alpha$ -sepiolite is used. Or both  $\alpha$ -sepiolite and  $\beta$ -sepiolite may be jointly used. The sepiolite is solidified when kneaded in water and is dried. At a temperature of 40 to 800°C, light sintering properties are obtained. In particular, the  $\alpha$ -sepiolite interlocks very well with ceramic fibers and vermiculite, and is not broken, unlike glass fibers and ceramic fibers, even though rubbed or tightened. Accordingly, the heat-resistant expansive sheet 2A containing the sepiolite prevents the occurrence of a negative expansion around 300°C under surface pressure loading. This improves the holding force to the ceramic honeycomb monolithic catalyst 1.

The treated vermiculite is obtained by treating particulate vermiculite with an aqueous solution of sodium ammonium hydrogen phosphate. The particulate vermiculite contains cations apt to be exchanged with  $\text{Na}^+$  ions and cations apt to be exchanged with  $\text{NH}_4^+$  ions. Accordingly, when the particulate vermiculite is immersed in the aqueous solution above-mentioned containing these both ions, the cations in the particulate vermiculite are effectively ion-exchanged in the aqueous solution. By such an ion exchange, the expansion amount and expansion force of the vermiculite are increased.

The ceramic fibers not only improve the heat resistance, but also prevent a negative expansion around  $300^\circ\text{C}$ . The ceramic fibers serve as a binder to improve the shape retention of the sheet particularly in a high-temperature zone where the organic binder perfectly disappears.

As the organic binder, there may be advantageously used a vinyl acetate-ethylene-acrylate copolymer, an acrylate polymer, cellulose pulp, a synthetic rubber (for example, NBR manufactured by Nippon Zeon Co., Ltd.), or the like. The vinyl acetate-ethylene-acrylate copolymer excellent in anchorage is preferred. The content of the organic binder should be within a range from 5 to 20 wt% because the flexibility at an ordinary temperature is insufficient at less than 5 wt%.

One thousand grs. of particulate vermiculite from South Africa was immersed in each of three different aqueous solutions as shown in Table 1 at an ordinary temperature for 120 hours. After washed with running water, each vermiculite was dried at  $105^\circ\text{C}$  for 2 hours and heated at a predetermined heating temperature for 30 minutes. Thereafter, its specific volume was measured with a measuring cylinder. The measurement results are shown in Table 2 and Fig. 3.

Table 1

| Treating Aqueous Solutions |                                    |                               |                             |
|----------------------------|------------------------------------|-------------------------------|-----------------------------|
| Treating Chemical          | Sodium ammonium hydrogen phosphate | Ammonium dihydrogen phosphate | Sodium dihydrogen phosphate |
| Amount(g)                  | 150                                | 150                           | 400                         |
| Water(g)                   | 850                                | 850                           | 800                         |

Table 2

| Expansion Degree of Vermiculite by Heat Treatment (Specific volume cc/g) |                                    |                               |                             |
|--|------------------------------------|-------------------------------|-----------------------------|
| Treating Solution  | Sodium ammonium hydrogen phosphate | Ammonium dihydrogen phosphate | Sodium dihydrogen phosphate |
| Heat Treatment   | Vermiculite No. 1                  | Vermiculite No. 1             | Vermiculite No. 1           |
| Unheated   | 1.1 (0)                            | 1.1 (0)                       | 0.9 (0)                     |
| 200 ° C  | 1.1 (0)                            | 0.9(-18)                      | 0.9 (0)                     |
| 225 ° C  | 1.1 (0)                            | 0.9(-18)                      | 0.9 (0)                     |
| 250 ° C  | 1.1 (0)                            | 0.9(-18)                      | 0.9 (0)                     |
| 275 ° C  | 1.6 (45)                           | 0.9(-18)                      | 0.9 (0)                     |
| 300 ° C  | 2.6 (136)                          | 0.9(-9)                       | 1.1 (22)                    |
| 325 ° C  | 2.9 (164)                          | 1.0(-9)                       | 1.9 (111)                   |
| 350 ° C  | 3.8 (245)                          | 1.6(45)                       | 2.8 (211)                   |
| 375 ° C  | 4.3 (291)                          | 2.4(118)                      | 3.3 (267)                   |
| 400 ° C  | 4.5 (309)                          | 2.9(164)                      | 3.3 (267)                   |
| 600 ° C  | 5.4 (391)                          | 5.1(364)                      | 4.2(367)                    |

In Table 2, the numerals in parenthesis represent thermal expansion coefficients in %. The vermiculite No. 1 has a grain size of 0.5 to 2 mm.

As shown in Table 2, the vermiculite treated with sodium ammonium hydrogen phosphate presented no shrinkage, i.e., negative expansion, at a temperature of 200 to 300 ° C as done in the vermiculite treated with ammonium dihydrogen phosphate. Further, the vermiculite treated with sodium ammonium hydrogen phosphate presented an expansion degree (expansion amount) higher than that of the vermiculite treated with sodium dihydrogen phosphate, and started expanding at a temperature as low as 275 ° C.

Two examples of the heat-resistant expansive sheet were manufactured by the beater seating method at the blending ratio of 4 wt% of  $\alpha$ -sepiolite, 54 wt% of each of treated vermiculites No. 0 and No. 1 as shown in Table 3, 30 wt% of ceramic fibers, and 12 wt% of a vinyl acetate-ethylene-acrylate copolymer as an organic binder. Each sheet thus formed had a thickness of 4.9 mm and density of 0.5 to 0.8 g/cm<sup>3</sup>, preferably 0.7 g/cm<sup>3</sup>. From each sheet, there was prepared a sample piece A having a diameter of 15 mm and a thickness of 4.9 mm. As shown in Fig. 2, each piece A was so compressed as to have a thickness of 3 mm by quartz rods 7A with the use of a load cell 6 in a heating furnace 5. There was measured the thermal expansion force of each piece A while the temperature was increased to 75 ° C for about 50 minutes. The results were shown in Table 3.

Table 3

| Thermal Expansion of Heat-Resistant Expansive Sheet (kgf) |             |             |
|---|-------------|-------------|
| Measured Grain Size of Vermiculite                        | No. 0       | No. 1       |
|   | 0.1 to 1 mm | 0.5 to 2 mm |
| Temp.   |             |             |
| 400 °C  | 4 kgf       | 7 kgf       |
| 500 °C  | 19 kgf      | 18 kgf      |
| 600 °C  | 39 kgf      | 38 kgf      |
| 700 °C  | 52 kgf      | 43 kgf      |
| 750 °C  | 54 kgf      | 42 kgf      |

It is apparent from Table 3, each sample piece A presents a high expansion force even in the high-temperature zone. In particular, the sheet using the vermiculite No. 0 having a smaller grain size, presents a higher expansion force and a smaller decrease in expansion force at a high temperature. Accordingly, such a sheet is suitable for a holding member for holding a ceramic catalyst in a motor vehicle or the like which is required to present a high expansion force even at a high temperature. The vermiculite No. 1 having a greater grain size is slightly inferior in expansion force to the vermiculite No. 0 having a smaller grain size. As shown in Table 2, however, the expansion amount of the vermiculite No. 1 depends on the treating aqueous solution used. Accordingly, the vermiculite No. 1 presenting a relatively great expansion amount may be suitably used for, for example, a refractory sealing material for covering the outer periphery of a power transmission line passing through a through-hole in a built wall.

Each cylindrical catalyst 10 having an outer diameter of 76 mm shown in Fig. 4 was surrounded, at the outer periphery thereof, by each of the heat-resistant expansive sheet 2A of the present invention and a conventional heat-resistant expansive sheet (Japanese Patent Publication 61-35143). Each catalyst-sheet assembly was loaded in a metallic cylindrical casing 11 having an inner diameter of 82.2 mm and subjected to a heat-treatment. Then, each cylindrical catalyst 10 was pushed in a direction shown by an arrow at a compression speed of 50 m/min. by a load cell 14 through a rubber plate 12 and a metallic plate 13. Thus, there was measured the pushing force required for pushing out each cylindrical catalyst 10, i.e., the holding force provided by each heat-resistant expansive sheet. The results are shown in Table 4 and a graph in Fig. 5.

Table 4

| Pushing Force Applied to Cylindrical Catalyst (kgf) |                |                 |                    |
|---|----------------|-----------------|--------------------|
|   |                | Invention Sheet | Conventional Sheet |
| Ordinary Temp.                                      | -              | 70              | 65                 |
| 225   | 6 hrs. or more | 92              | 62                 |
| 325   | "              | 59              | 12                 |
| 425   | "              | 72              | 55                 |
| 600   | "              | 92              | 62                 |
| 800   | "              | 300             | 180                |

It is apparent from Table 4 and the graph in Fig. 5 that the conventional heat-resistant expansive sheet

is considerably decreased in holding force at 325° C due to the negative expansion mentioned earlier, and presents a small holding force at a high temperature of 600° C or more. It is also apparent that the heat-resistant expansive sheet 2A of the present invention presents no considerable decrease in holding force even in a negative expansion zone at 325° C, and assures a great holding force in a high-temperature zone of 600° C or more. It may be considered that such effects of the present invention have been produced by the synergistic effect of the respective expansion amounts and respective expansion forces of the vermiculite treated with sodium ammonium hydrogen phosphate and the sepiolite which was not contained in the conventional sheet.

The heat-resistant expansive sheet 2B in accordance with a second invention may be manufactured by the beater seating method at the blending ratio of 21 to 30 wt% of sepiolite, 30 to 40 wt% of vermiculite treated with sodium ammonium hydrogen phosphate, 20 to 40 wt% of ceramic fibers, and 5 to 20 wt% of an organic binder.

According to the heat-resistant expansive sheet 2B, the blending ratio of sepiolite is considerably increased as compared with the heat-resistant expansive sheet 2A, thereby to improve the heat resistance in a high-temperature zone. Further, the blending ratio of the treated vermiculite is slightly lowered, thereby to slightly restrain the expansion amount and expansion force of the heat-resistant expansive sheet 2B.

Thus, the heat-resistant expansive sheet 2A of the first invention having a greater expansion amount and a greater expansion force than those of the heat-resistant expansive sheet 2B of the second invention, may be suitable for a holding member of a catalyst converter having great rigidity mounted on the exhaust system of a four-wheel motor vehicle. On the other hand, the heat-resistant expansive sheet 2B of the second invention may be suitable for a holding member of a catalyst converter mounted on the exhaust system of a two-wheel motor vehicle, i.e., a catalyst converter of which rigidity is slightly lower than that of the catalyst converter for a four-wheel motor vehicle. In other words, as compared with the catalyst converter for a four-wheel motor vehicle, the catalyst converter for a two-wheel motor vehicle presents smaller rigidity since the compressive strength of the honeycomb monolithic catalyst 1 is smaller and the metallic casing 3 is thinner. However, when the heat-resistant expansive sheet 2B of which expansion amount and expansion force are being restrained, is used for the catalyst converter for a two-wheel motor vehicle, it is possible to prevent the monolithic catalyst 1 from being broken and the metallic casing 3 from being abnormally deformed due to excessive expansion.

By the beater seating method, there were manufactured, at the blending ratios set forth in Table 5, examples of the heat-resistant expansive sheets 2A, 2B of the present invention each having a thickness of 4.9 mm, a width of 25 mm, a length of 25 mm, and density of 0.5 to 0.8 g/cm<sup>3</sup>, preferably 0.7 g/cm<sup>3</sup>. There was also manufactured a conventional heat-resistant expansive sheet having the same dimensions and density as those of the sheets of the present invention. There were measured the gas-attack resisting properties of such sheets 2A, 2B and the conventional sheet, with the use of a gas-attack resisting property testing apparatus shown in Figs. 6 and 7. The test results are shown in Table 6.

The gas-attack resisting property testing apparatus in Figs. 6 and 7, includes two plates 51 between and by which each heat-resistant expansive sheet is held through a plurality of gap spacers 50, and a flat nozzle 52 to be reciprocated (with a traverse amount of 19.1 mm), as facing the end surface of each heat-resistant expansive sheet, at a speed of 20 cycles/min. in a direction y. This nozzle 52 is adapted to blow air of 2.5 kgf/cm<sup>2</sup>. The test was conducted according to a pattern of (i) heating at 600° C for one hour, (ii) cooling, (iii) measurement of the weight, (iv) blowing of air in 3000 cycles, (v) measurement of the weight, (vi) blowing of air in 3000 cycles, and (vii) measurement of the weight.

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Table 5

| Blending Ratio in Heat-Resistant Expansive Sheet (wt%) |                                      |                                      |
|--|--------------------------------------|--------------------------------------|
|  | Heat-Resistant<br>Expansive Sheet 2A | Heat-Resistant<br>Expansive Sheet 2B |
| Vermiculite  | 54                                   | 37                                   |
| Sepiolite  | 4                                    | 21                                   |
| Ceramic Fibers (alumina, silicate)                     | 30                                   | 30                                   |
| Organic Binder*  | 12                                   | 12                                   |

\* Vinyl acetate-ethylene-acrylate copolymer

Table 6

| Weight Decrease of Heat-Resistant Expansive Sheet (%) |                       |                       |                       |
|---|-----------------------|-----------------------|-----------------------|
|   | Invention<br>Sheet 2A | Invention<br>Sheet 2B | Conventional<br>Sheet |
| After 3000 Cycles                                     | 5.5                   | 0.9                   | 28                    |
| After 6000 Cycles                                     | 6.5                   | 1.1                   | 33                    |

It is apparent from Table 6 that each of the heat-resistant expansive sheets of the present invention presents remarkably excellent gas-attack resisting properties as compared with the conventional sheet. It is therefore possible to prevent the heat-resistant sheet of the present invention from being lowered in holding performance with the passage of time. This may be considered to be achieved by improvements in shape retention due to presence of sepiolite.

The heat-resistant expansive sheet 2B having a higher blending amount of sepiolite is superior in gas-attack resisting properties to the heat-resistant expansive sheet 2A. Accordingly, the heat-resistant expansive sheet 2B excellent in gas-attack resisting properties is suitable for a holding member for the exhaust system of a two-wheel motor vehicle in which the distance between the engine exhaust port and the catalyst converter is short and the catalyst converter is therefore exposed to the exhaust gas flowing at a high speed so that the heat-resistant expansive sheet is susceptible to severe gas attack. On the other hand, the heat-resistant expansive sheet 2A is suitable for a holding member for the exhaust system of a four-wheel motor vehicle in which the distance between the engine exhaust port and the catalyst converter is long and the catalyst converter is therefore exposed to the exhaust gas of which speed is being slightly lowered, so that the gas attack to the heat-resistant expansive sheet is relatively small.

#### Claims

1. A heat-resistant expansive member comprising 1 to 5 wt% of sepiolite, 30 to 60 wt% of treated vermiculite, 20 to 40 wt% of ceramic fibers and 5 to 20 wt% of an organic binder.

2. A heat-resistant expansive member according to Claim 1; wherein the treated vermiculite is obtained by treating particulate vermiculite with an aqueous solution of sodium ammonium hydrogen phosphate.

3. A heat-resistant expansive member according to Claim 2, wherein the particulate vermiculite has a grain size of 0.5 to 2 mm.

4. A heat-resistant expansive member according to Claim 2, wherein the particulate vermiculite has a grain size of 0.1 to 1 mm.

5. A heat-resistant expansive member according to Claim 1, wherein the sepiolite is  $\alpha$ -type sepiolite.

6. A heat-resistant expansive member according to Claim 1, wherein the sepiolite is contained as a mixture of  $\alpha$ -type sepiolite and  $\beta$ -type sepiolite.

7. A heat-resistant expansive member according to Claim 1, wherein the organic binder is a vinyl acetate-ethylene-acrylate copolymer.
8. A heat-resistant expansive member according to Claim 2, wherein the organic binder is a vinyl acetate-ethylene-acrylate copolymer.
- 5 9. A heat-resistant expansive member according to Claim 1, wherein the organic binder is selected from the group consisting of an acrylate polymer, cellulose pulp and synthetic rubber.
10. A heat-resistant expansive member according to Claim 1, made at the blending ratio of 4 wt% of  $\alpha$ -type sepiolite, 54 wt% of treated vermiculite, 30 wt% of ceramic fibers, and 12 wt% of a vinyl acetate-ethylene-acrylate copolymer as the organic binder.
- 10 11. A heat-resistant expansive member according to Claim 10, made by the beater seating method and having density of 0.5 to 0.8 g/cm<sup>3</sup>.
12. A heat-resistant expansive member according to Claim 11, wherein the treated vermiculite is obtained by treating particulate vermiculite with an aqueous solution of sodium ammonium hydrogen phosphate.
- 15 13. A heat-resistant expansive member comprising 21 to 30 wt% of sepiolite, 30 to 40 wt% of treated vermiculite, 20 to 40 wt% of ceramic fibers and 5 to 20 wt% of an organic binder.
14. A heat-resistant expansive member according to Claim 13, wherein the treated vermiculite is obtained by treating particulate vermiculite with an aqueous solution of sodium ammonium hydrogen phosphate.
- 20 15. A heat-resistant expansive member according to Claim 14, wherein the particulate vermiculite has a grain size of 0.5 to 2 mm.
16. A heat-resistant expansive member according to Claim 14, wherein the particulate vermiculite has a grain size of 0.1 to 1 mm.
17. A heat-resistant expansive member according to Claim 13, wherein the sepiolite is  $\alpha$ -type sepiolite.
- 25 18. A heat-resistant expansive member according to Claim 13, wherein the sepiolite is contained as a mixture of  $\alpha$ -type sepiolite and  $\beta$ -type sepiolite.
19. A heat-resistant expansive member according to Claim 13, wherein the organic binder is a vinyl acetate-ethylene-acrylate copolymer.
20. A heat-resistant expansive member according to Claim 14, wherein the organic binder is a vinyl acetate-ethylene-acrylate copolymer.
- 30 21. A heat-resistant expansive member according to Claim 13, wherein the organic binder is selected from the group consisting of an acrylate polymer, cellulose pulp and synthetic rubber.
22. A heat-resistant expansive member according to Claim 13, made at the blending ratio of 21 wt% of  $\alpha$ -type sepiolite, 37 wt% of treated vermiculite, 30 wt% of ceramic fibers, and 12 wt% of a vinyl acetate-ethylene-acrylate copolymer as the organic binder.
- 35 23. A heat-resistant expansive member according to Claim 22, made by the beater seating method and having density of 0.5 to 0.8 g/cm<sup>3</sup>.
24. A heat-resistant expansive member according to Claim 23, wherein the treated vermiculite is obtained by treating particulate vermiculite with an aqueous solution of sodium ammonium hydrogen phosphate.
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Fig.1

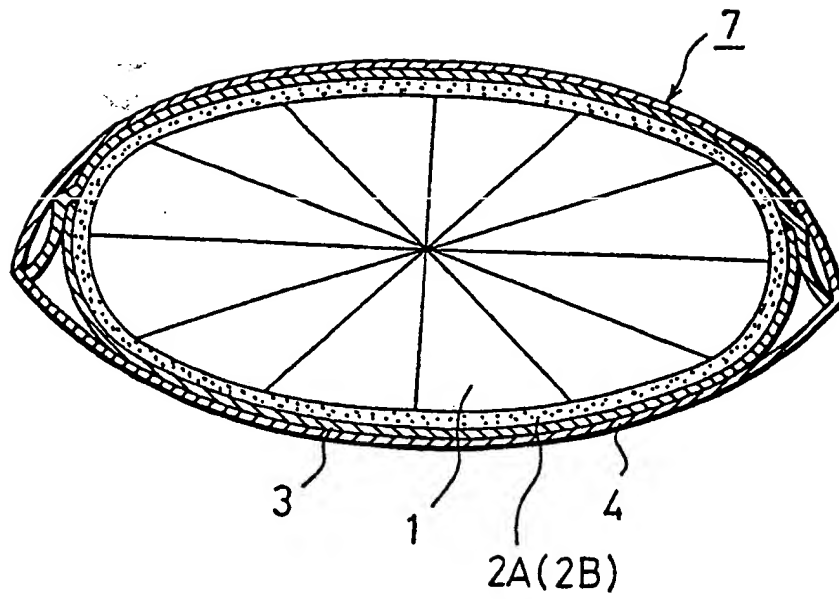


Fig.2

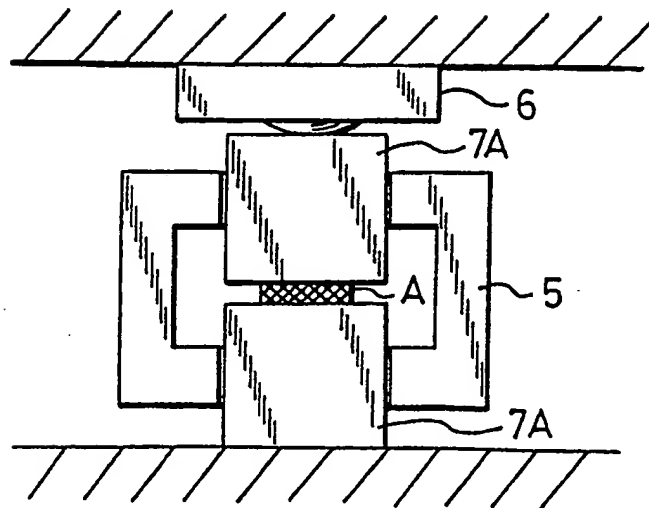


Fig.3

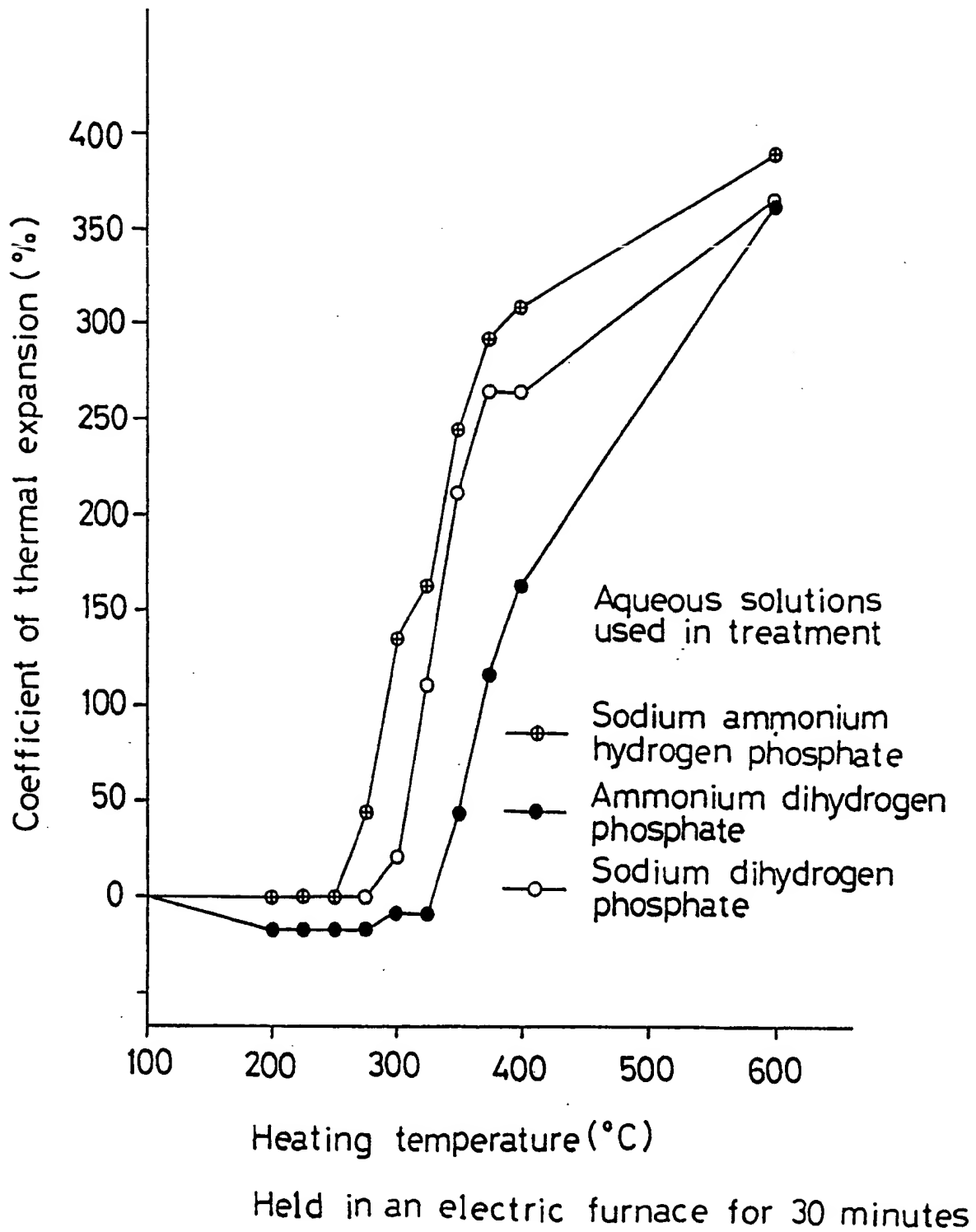


Fig.4

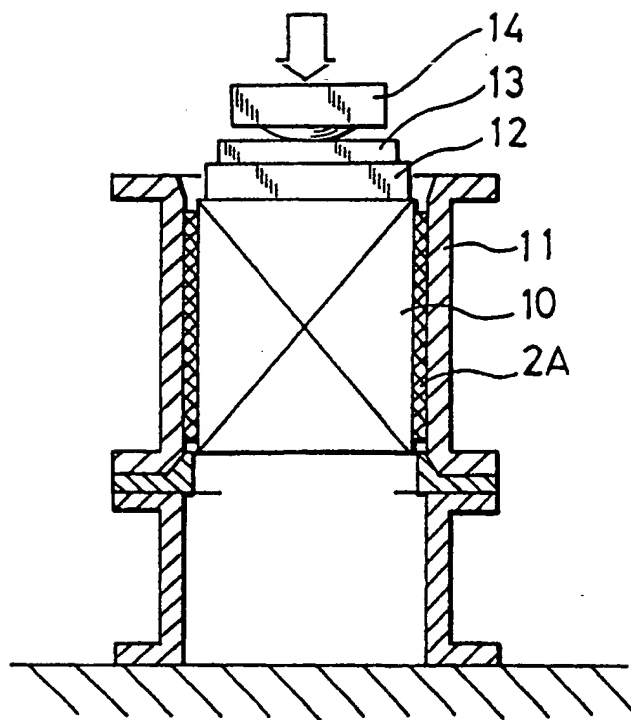


Fig.5

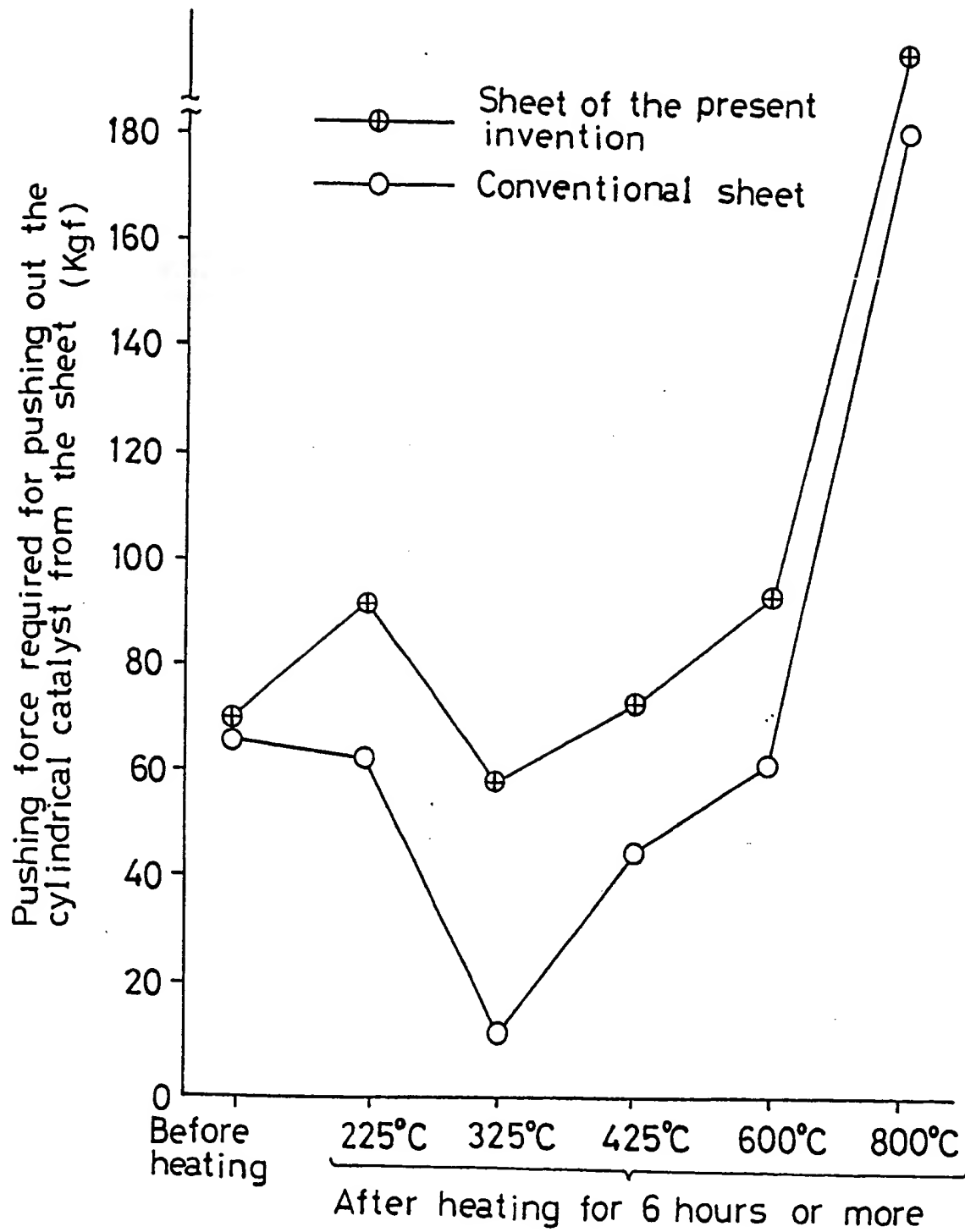


Fig.6

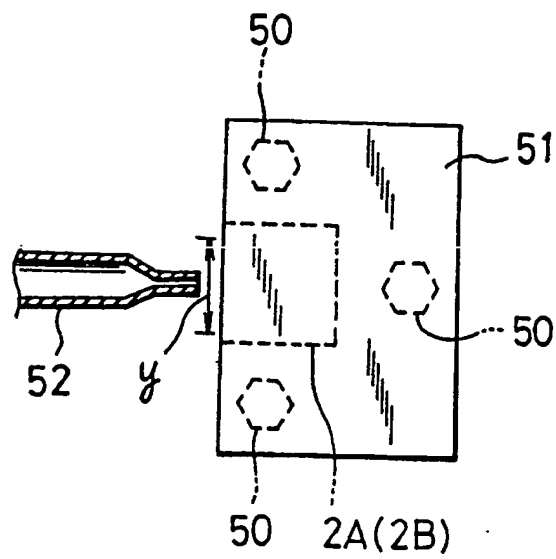
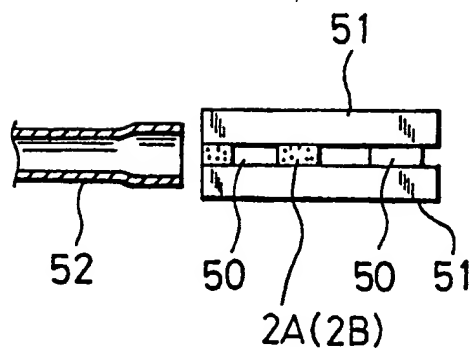


Fig.7



(19)



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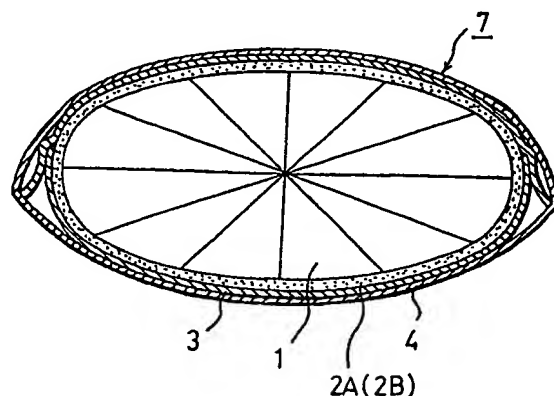
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(12)

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**W-8000 München 71(DE)**(54) **Heat-resistant expansive member.**

(57) The present invention relates to a heat-resistant expansive member suitably used as a holding member for holding a ceramic monolithic catalyst in a motor vehicle or the like. The heat-resistant expansive member of the present invention is made at the blending ratio of 1 to 5 wt% of sepiolite, 30 to 60 wt% of treated vermiculite, 20 to 40 wt% of ceramic fibers and 5 to 20 wt% of an organic binder, or at the blending ratio of 21 to 30 wt% of sepiolite, 30 to 40 wt% of treated vermiculite, 20 to 40 wt% of ceramic fibers and 5 to 20 wt% of an organic binder. Regardless of the low- or high-temperature zone, the heat-resistant expansive member of the present invention presents a great holding force to the monolithic catalyst or the like. The heat-resistant expansive member is improved in cushioning properties and gas-attack resisting properties particularly in the high-temperature zone.

Fig.1







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# EUROPEAN SEARCH REPORT

Application Number

EP 90 10 8655

| DOCUMENTS CONSIDERED TO BE RELEVANT   |  |  |   |
|---|--|--|---|
| Category  | Citation of document with indication, where appropriate, of relevant passages              | Relevant to claim                              | CLASSIFICATION OF THE APPLICATION (Int. Cl.5)                               |
| A,P   | US-A-4 865 818 (R.P. MERRY et al.)<br>* column 3, lines 3-23; claims 1-8 *<br>- - -        | 1-4,7-10,<br>12-16                             | F 01 N 3/28<br>F 01 N 3/24  |
| A,P   | EP-A-0 328 293 (MINNESOTA MINING AND MANUFACTURING COMPANY)<br>* claims 1,4-9 *<br>- - -   | 1-4  |   |
| A   | EP-A-0 030 123 (MINNESOTA MINING AND MANUFACTURING COMPANY)<br>* claims 1,2 *<br>- - - - - | 1-4  |   |
| The present search report has been drawn up for all claims  |  |  | TECHNICAL FIELDS<br>SEARCHED (Int. Cl.5)<br><br>B 01 D 53/00<br>F 01 N 3/00 |
| Place of search<br><br>Berlin   |  | Date of completion of search<br><br>10 July 91 | Examiner<br><br>BERTRAM H E H   |
| <div>CATEGORY OF CITED DOCUMENTS</div> <div>X: particularly relevant if taken alone<br/>Y: particularly relevant if combined with another document of the same category<br/>A: technological background<br/>O: non-written disclosure<br/>P: intermediate document<br/>T: theory or principle underlying the invention</div> <div>E: earlier patent document, but published on, or after the filing date<br/>D: document cited in the application<br/>L: document cited for other reasons<br/>-----<br/>&amp;: member of the same patent family, corresponding document</div> |  |  |   |